

# IIR Filter Design

EE4015 Digital Signal Processing

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- IIR Digital Filter Design Methods
  - Impulse Invariance Method
  - Bilinear Transformation Method
  - Frequency Band Transformation

# IIR Digital Filter Design Methods

- Analog-to-Digital Transformations
- Digital-to-Digital Transformations

- Impulse Invariance

- $H_a(s) \rightarrow h(t) \xrightarrow{\text{sampling}} h[n] \rightarrow H(z)$

- Bilinear Transformation

- $H_a(s) \xrightarrow{s = \frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}} H(z)$

- Frequency Band Transformation

- $H(z) \xrightarrow{z^{-1} = \frac{z^{-1}-a}{1-az^{-1}}} H(z)$

- Pole-zero placement method

$$H(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_{M-1} z^{M-1} + b_M z^M}{a_0 + a_1 z^{-1} + \dots + a_{N-1} z^{N-1} + b_N z^N}$$

# Analog-to-Digital Filter Transformation

- Some of the IIR filters design methods are to apply a transformation to an **existing analog filter** to obtain the digital filter transfer functions, such as

$$H_a(s) = \frac{1}{s - a} \xleftrightarrow{\text{Transformation}} H(z) = \frac{1}{1 - bz^{-1}}$$

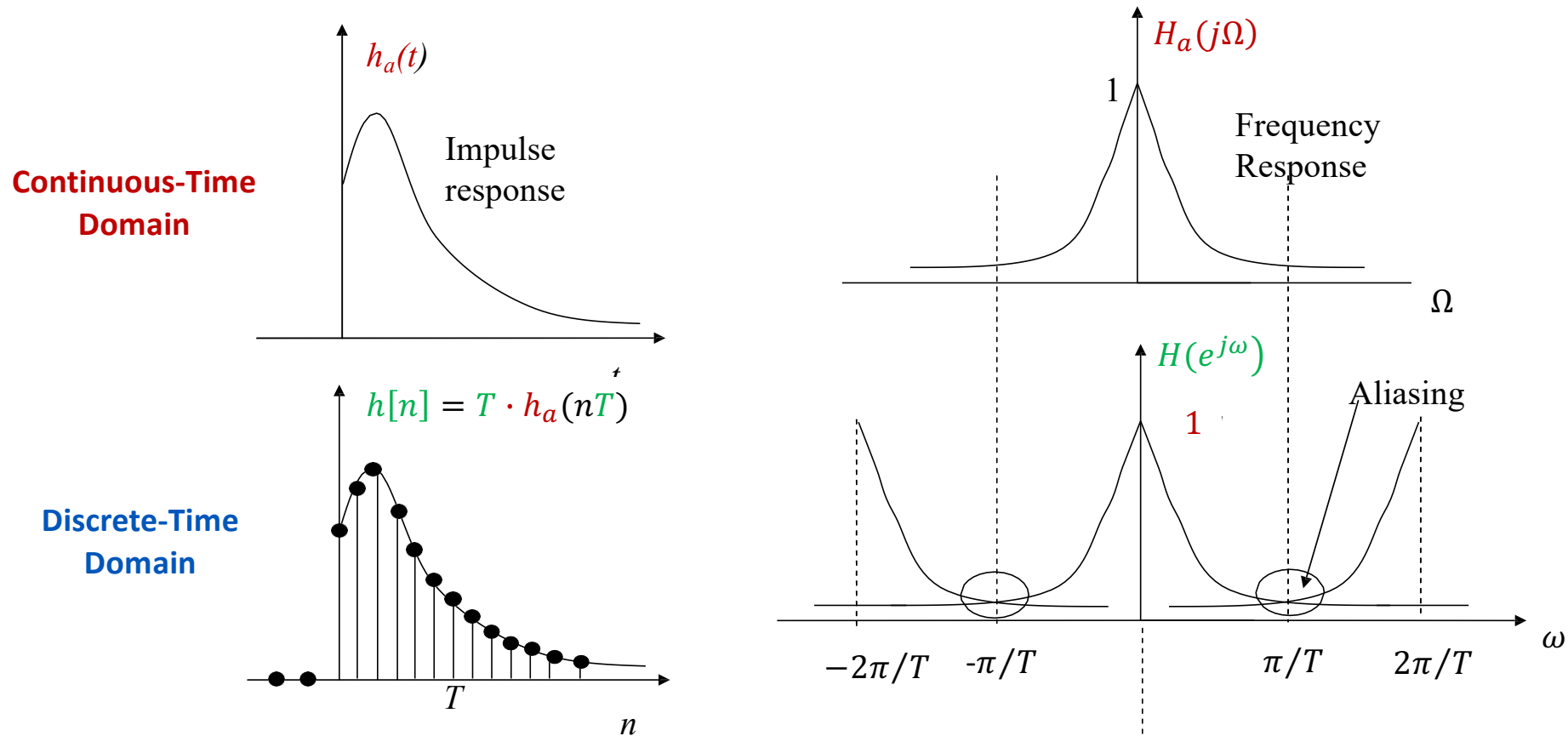
- Their common feature is that a **stable analog filter will transform to a stable discrete-time system** with transfer function  $H(z)$ .
- Left half of  $s$ -plane maps into inside of unit circle in  $z$ -plane

# Impulse Invariance Method

# Impulse Invariance Method

- This method starts from an analog filter's transfer function  $H_a(s)$  to obtain its impulse response  $h_a(t)$  by inverse Laplace Transform.
- The objective of the design is to realize an IIR filter with an impulse response  $h[n]$  which satisfies :
  - $h[n] = T \cdot h_a(nT)$  where  $T$  is the sampling period ( $T = 1/F_s$ )
- Finally, use z-Transform to obtain  $H(z)$  with filter coefficients from the sampled impulse response  $h[n]$ .
- The main feature of this method is that the impulse response  $h[n]$  of the resulting digital filter is a sampled version of the impulse response  $h_a(t)$  of the analog filter.

# Sampling of the Impulse Response



- The problem of Impulse Invariance is sensitivity to the choice of  $T$ . Too large  $T$  will create aliasing problem to distorting the frequency response of the IIR digital Filter.

# Spectrum of the Sampled Impulse Response

- With the use of convolution property,  $H(e^{j\omega})$  is

$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} H_a \left( j \left( \frac{\omega}{T} - \frac{2\pi k}{T} \right) \right)$$

- Where the analog and digital frequencies

$$\omega = \Omega T$$

- The impulse response of the resultant IIR filter is similar to that of the analog filter
- Aliasing due to the overlapping of  $\left\{ H_a \left( j \left( \frac{\omega}{T} - \frac{2\pi k}{T} \right) \right) \right\}$  which are **not bandlimited**.



# Impact of the Sampling Frequency

- The sampling frequency affects the frequency response of the impulse invariant discrete filter.
- **A sufficient high sampling frequency is necessary** for the frequency response to be close to that of the equivalent analog filter.
- Due to aliasing, therefore, the frequency response of the digital filter will **not be identical to that of the analog filter**.

# Derive Transfer Function $H(z)$ (1)

- To derive the IIR filter transfer function  $H(z)$  from  $H_a(s)$ , we first obtain the partial fraction expansion:

$$H_a(s) = \sum_{k=1}^N \frac{A_k}{s - c_k}$$

where  $\{c_k\}$  are the poles on the left half of the s-plane

- The inverse Laplace transform of  $H_a(s)$  is given as:

$$h_a(t) = \begin{cases} \sum_{k=1}^N A_k e^{c_k t}, & t \geq 0 \\ 0, & t < 0 \end{cases} = \left( \sum_{k=1}^N A_k e^{c_k t} \right) u(t)$$

## Derive Transfer Function $H(z)$ (2)

- Sample and scale  $h_a(t)$  with period  $T$  to obtain  $h[n]$  :

$$h[n] = \sum_{k=1}^N T A_k e^{c_k T n} u[n]$$

- The z-transform of  $h[n]$  is

$$H(z) = \sum_{k=1}^N \frac{T A_k}{1 - e^{c_k T} z^{-1}}$$

# Relationship between $H_a(s)$ and $H(z)$

$$H_a(s) = \sum_{k=1}^N \frac{A_k}{s - c_k} \quad \longrightarrow \quad H(z) = \sum_{k=1}^N \frac{TA_k}{1 - e^{c_k T} z^{-1}}$$

- It can be seen that a pole of  $s = c_k$  in the s-plane transforms to a pole at  $z = e^{c_k T}$  in the z-plane:

$$z = e^{sT}$$

- Expressing  $s = \sigma + j\Omega$

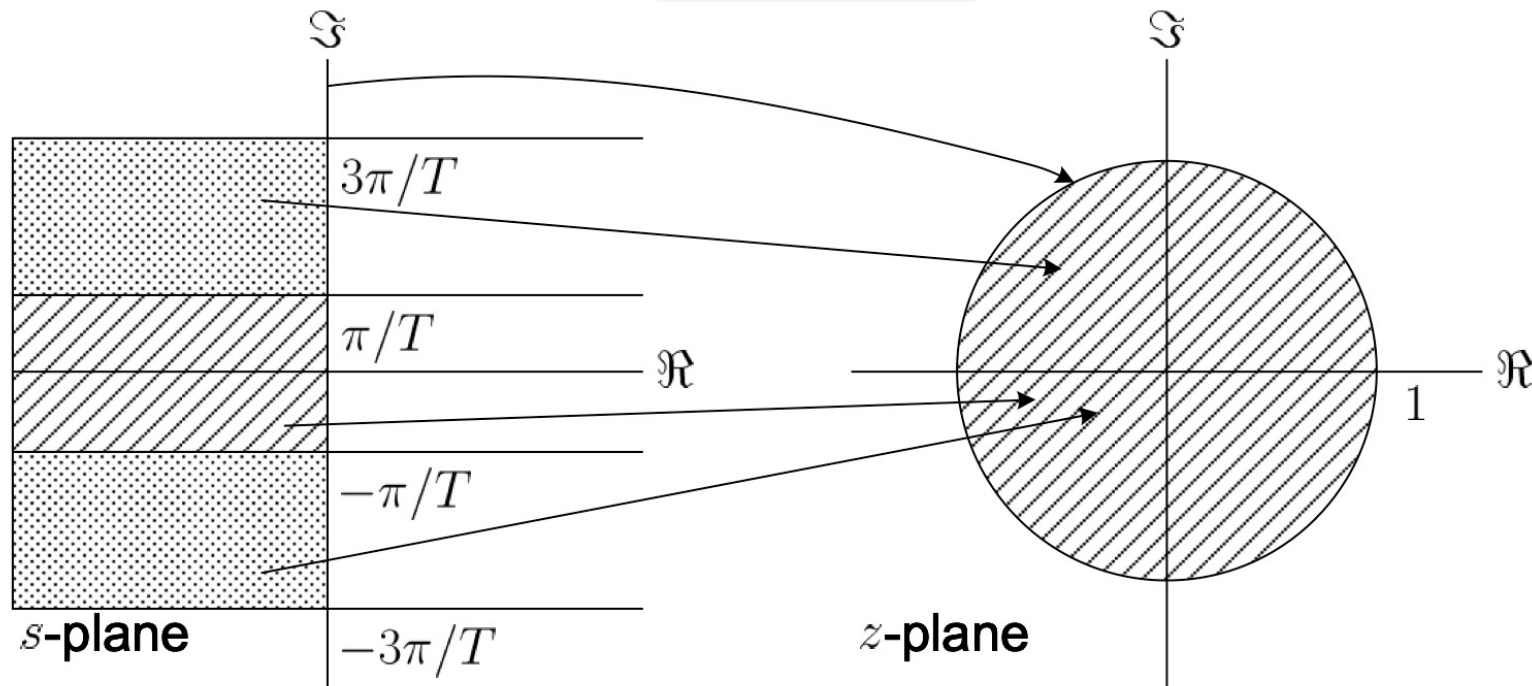
$$z = e^{\sigma T} \cdot e^{j\Omega T} = e^{\sigma T} \cdot e^{j(\Omega + 2\pi k/T)T}$$

where  $k$  is any integer, indicating a many-to-one mapping

- Each infinite horizontal strip of with  $2\pi/T$  maps into the entire z-plane

# Mapping between $s$ and $z$ in Impulse Invariance Method

$$z = e^{sT}$$



# Stability of Impulse Invariance Method

- $\sigma = 0$  maps to  $|z| = 1$  , that is,  $j\Omega$  axis in the s-plane transforms to the unit circle in the z-plane
- $\sigma < 0$  maps to  $|z| < 1$  , left half of the s-plane maps into the inside of the unit circle in the z-plane. Then, stable  $H_a(s)$  produces stable  $H(z)$
- $\sigma > 0$  maps to  $|z| > 1$  , right half of the s-plane maps into the outside of the unit circle in the z-plane

# Procedure of Impulse Invariance Method

Given the magnitude square response specifications of  $H(e^{j\omega})$  in terms of  $\omega_p$ ,  $\omega_s$ ,  $R_p$  and  $A_s$ , the design procedure for  $H(z)$  can be summarized as :

1. Select a value for the sampling interval  $T$  and then compute the passband and stopband frequencies for the analog lowpass filter according to  $\Omega_p = \omega_p/T$  and  $\Omega_s = \omega_s/T$
2. Design the analog Butterworth filter with transfer function  $H_a(s)$  according to  $\Omega_p$ ,  $\Omega_s$ ,  $R_p$  and  $A_s$
3. Perform partial fraction expansion on  $H_a(s) = \sum_{k=1}^N \frac{A_k}{s-c_k}$
4. Obtain  $H(z)$  by

$$H(z) = \sum_{k=1}^N \frac{TA_k}{1 - e^{c_k T} z^{-1}}$$

# Impulse Invariance Method Example 1

$$H(s) = \frac{1}{(s+1)(s+3)}$$

- Using partial fraction this can be written as

$$H(s) = \frac{0.5}{s+1} - \frac{0.5}{s+3}$$

$$\downarrow \frac{A}{s-c} \rightarrow \frac{AT}{1-e^{cT}z^{-1}}$$

$$H(z) = \frac{0.5T}{1-e^{-T}z^{-1}} - \frac{0.5T}{1-e^{-3T}z^{-1}} = \frac{0.5T(e^{-T} - e^{-3T})z^{-1}}{1 - (e^{-T} - e^{-3T})z^{-1} + e^{-4T}z^{-2}}$$



## Impulse Invariance Method Example 2

- Determine the transfer function  $H(z)$  of a digital lowpass filter whose magnitude requirements are  $\omega_p = 0.4\pi$ ,  $\omega_s = 0.6\pi$ ,  $R_p = 8 \text{ dB}$  and  $A_s = 16 \text{ dB}$ .
- Use the Butterworth lowpass filter and **Impulse Invariance** Method with sampling interval  $T = 0.1$  in the design.

## Example 2 Solution

- With  $T = 0.1$ , the analog frequency parameters can be determined as

$$\Omega_p = \frac{\omega_p}{T} = 4\pi \quad \text{and} \quad \Omega_s = \frac{\omega_s}{T} = 6\pi$$

- Based on the example 2 in analog filter design results with  $\Omega_c = 10$ , we know the 3<sup>rd</sup> order Butterworth filter can meet the magnitude requirements and its transfer function is

$$H_a(s) = \frac{1}{(s^2 + s + 1)(s + 1)} \Big|_{s=\frac{s}{\Omega_c}} = \frac{1000}{(s^2 + 10s + 100)(s + 10)}$$

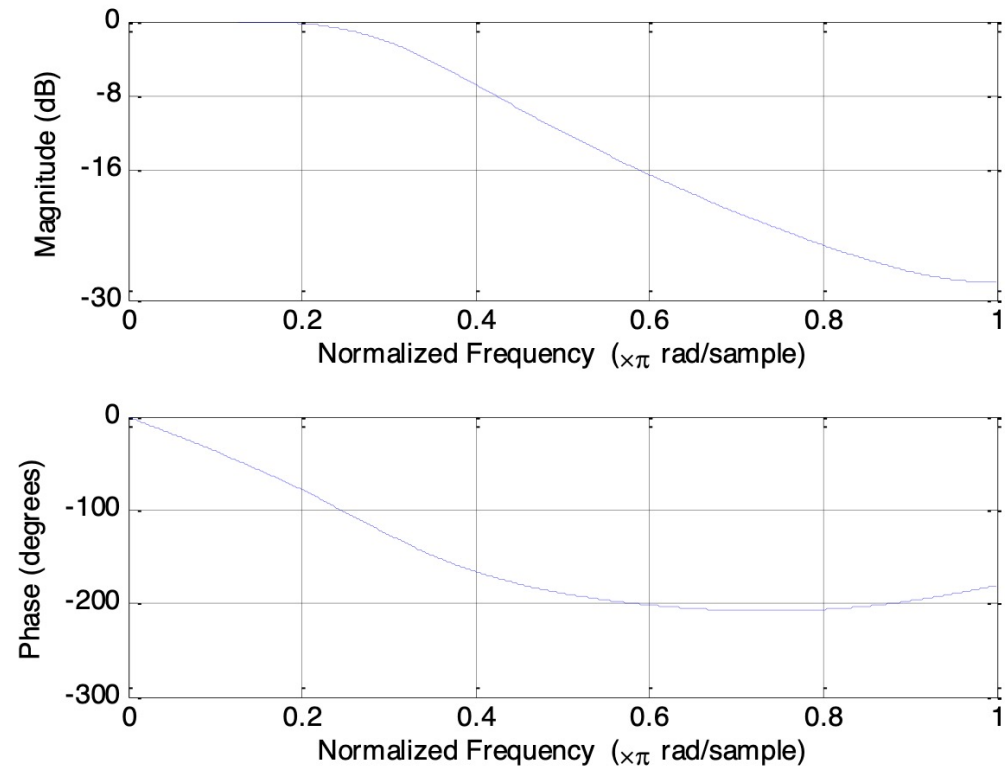
- Performing partial fraction expansion on  $H_a(s)$ , we have

$$H_a(s) = \frac{10}{s + 10} + \frac{-5 - j2.8868}{s + 5 - j8.6603} + \frac{-5 + j2.8868}{s + 5 + j8.6603}$$

- Using the mapping of  $H(z) = \sum_{k=1}^N \frac{TA_k}{1 - e^{c_k T} z^{-1}}$ , the transfer function of IIR filter is

$$\begin{aligned}
 H(z) &= \frac{0.1 \cdot 10}{1 - e^{-10 \cdot 0.1} z^{-1}} + \frac{0.1 \cdot (-5 - j2.8868)}{1 - e^{(-5 + j8.6603) \cdot 0.1} z^{-1}} + \frac{0.1 \cdot (-5 + j2.8868)}{1 - e^{(-5 - j8.6603) \cdot 0.1} z^{-1}} \\
 &= \frac{1}{1 - 0.3679z^{-1}} + \frac{-0.5 - j0.2887}{1 - (0.3929 + j0.4620)z^{-1}} + \frac{-0.5 + j0.2887}{1 - (0.3929 - j0.4620)z^{-1}} \\
 &= \frac{1}{1 - 0.3679z^{-1}} + \frac{-1 + 0.6597z^{-1}}{1 - 0.7859z^{-1} + 0.3679z^{-2}} \\
 &= \frac{0.2417z^{-1} + 0.1262z^{-2}}{1 - 1.1538z^{-1} + 0.6570z^{-2} - 0.1354z^{-3}}
 \end{aligned}$$

# Magnitude and phase responses based on impulse invariance Method

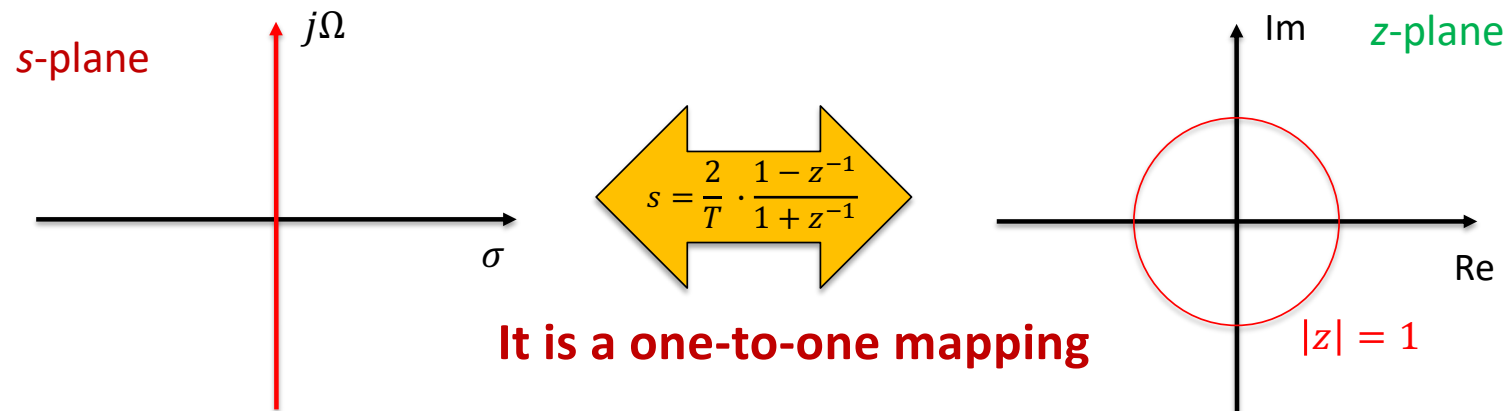


# **Bilinear Transformation Method**

# Bilinear Transformation Method

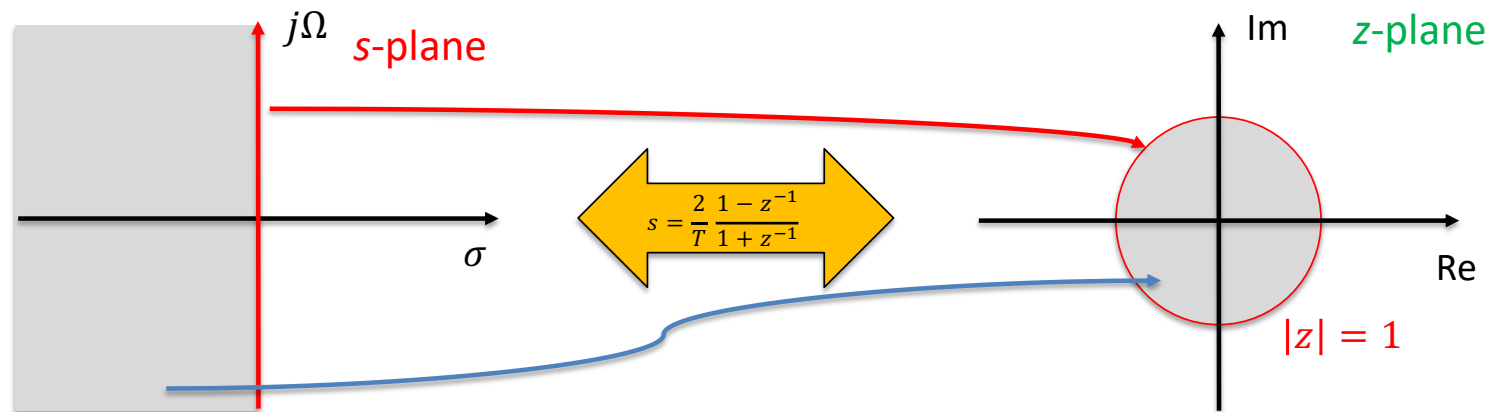
- Map continuous-time systems to discrete-time system by relating  $s$  and  $z$

$$z = e^{sT} = \frac{e^{\frac{sT}{2}}}{e^{-\frac{sT}{2}}} = \frac{1 + \frac{sT}{2} + \left(\frac{sT}{2}\right)^2 \cdot \frac{1}{2} + \dots}{1 - \frac{sT}{2} + \left(\frac{sT}{2}\right)^2 \cdot \frac{1}{2} + \dots} \Rightarrow z \approx \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}} \Rightarrow \boxed{s = \frac{2}{T} \cdot \frac{1 - z^{-1}}{1 + z^{-1}}}$$



# Bilinear Transformation Property 1

- Left half of s-plane ( $\sigma < 0$ ) maps to interior of unit circle in the z-plane



$$z = \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}} = \frac{1 + \frac{T}{2}\sigma + j\frac{T}{2}\Omega}{1 - \frac{T}{2}\sigma - j\frac{T}{2}\Omega}$$

$$\text{if } \begin{matrix} \sigma < 0, & |z| < 1 \\ \sigma > 0, & |z| > 1 \end{matrix}$$

- Stable Continuous-Time Systems  $\Leftrightarrow$  Stable Discrete-time Systems

# Bilinear Transformation Property 2

- $j\Omega$  axis maps to unit circle via a nonlinear warping

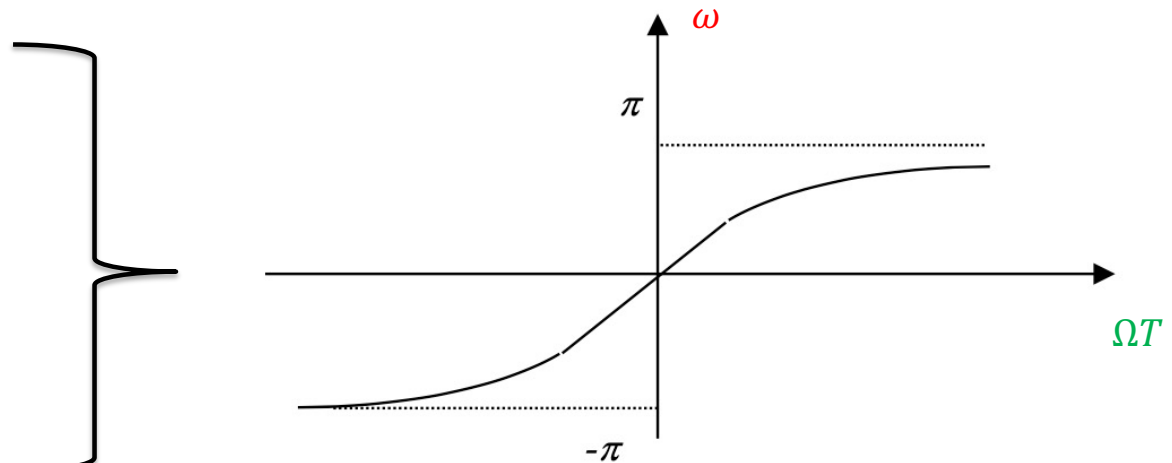
$$z = \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}} \xrightarrow{s=j\Omega} z = \frac{1 + j\frac{T}{2}\Omega}{1 - j\frac{T}{2}\Omega} \xrightarrow{|z|=1} e^{j\omega} = \frac{1 + j\frac{T}{2}\Omega}{1 - j\frac{T}{2}\Omega} \Rightarrow j\Omega = \frac{2}{T} \frac{1 - e^{-j\omega}}{1 + e^{-j\omega}} = \frac{2}{T} \frac{2je^{-\frac{j\omega}{2}} \sin \frac{\omega}{2}}{2je^{-\frac{j\omega}{2}} \cos \frac{\omega}{2}} = j \frac{2}{T} \tan \frac{\omega}{2}$$

Then, we have

$$\Omega = \frac{2}{T} \tan \frac{\omega}{2}$$

and

$$\omega = 2 \tan^{-1} \left( \frac{\Omega T}{2} \right)$$

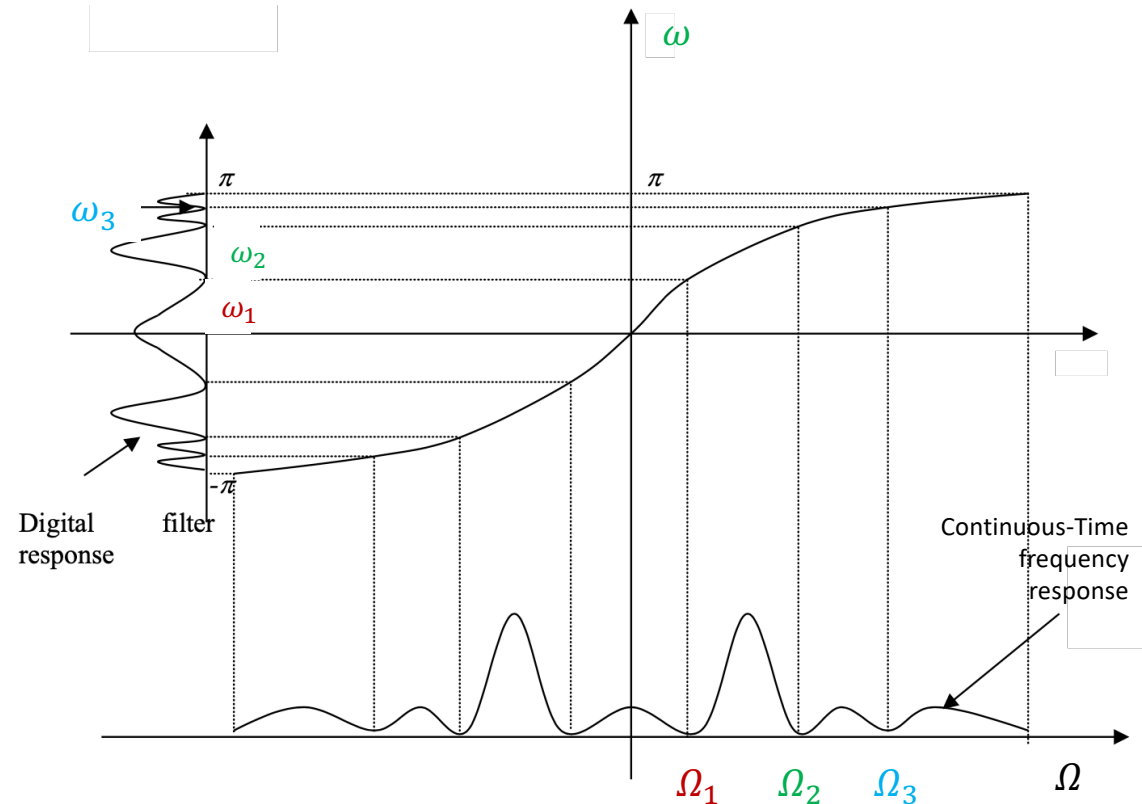


We see that a nonlinear relation exists between  $\Omega$  and  $\omega$ . This effect is called 'Warping'.



# Pro and Con of Frequency Warping

- **No aliasing of the frequency characteristic** can occur in the transformation of an analog filter to a discrete filter
- We must however **check carefully just how the various characteristic frequencies** of the continuous characteristic frequencies of the discrete filter.
- In designing a digital filter by this method, we must **first prewarp** the given filter specifications to find the continuous filter to which we are going to apply the bilinear transformation.



# Procedure of Bilinear Method

Given the magnitude square response specifications of  $H_{LP}(e^{j\omega})$  in terms of  $\omega_p$ ,  $\omega_s$ ,  $R_p$  and  $A_s$ , the design procedure for  $H(z)$  can be summarized as :

1. Select a value for the sampling interval  $T$  and then compute the passband and stopband frequencies for the analog lowpass filter according to  $\Omega_p = \frac{2}{T} \tan \frac{\omega_p}{2}$  and  $\Omega_s = \frac{2}{T} \tan \frac{\omega_s}{2}$
2. Design the analog filter with transfer function  $H_a(s)$  according to  $\Omega_p$ ,  $\Omega_s$ ,  $R_p$  and  $A_s$
3. Obtain  $H(z)$  from  $H_a(s)$  by the bilinear transformation

$$H(z) = H_a(s) \Big|_{s = \frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}}$$

# Bilinear Transformation Example 1

$$H_{LP}(s) = \frac{2s}{s^2 + 6s + 8}$$

- Using the bilinear transformation with  $T = 1$  to transform to a digital filter with transfer function  $H(z)$

$$\begin{aligned} H(z) &= \frac{2s}{s^2 + 6s + 8} \Big|_{s = \frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}} = \frac{2 \cdot 2 \frac{1-z^{-1}}{1+z^{-1}}}{\left(2 \frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 6 \cdot 2 \frac{1-z^{-1}}{1+z^{-1}} + 8} \\ &= \frac{4 - 4z^{-2}}{15 + 14z^{-1} + 9z^{-2}} = \frac{0.2667 - 40.2667z^{-2}}{1 + 0.933z^{-1} + 0.6z^{-2}} \end{aligned}$$

# Bilinear Transformation Example 2

- Determine the transfer function  $H_{LP}(z)$  of a digital lowpass filter with
  - Sampling frequency  $F_s$  : 8kHz
  - Passband edge frequency  $f_p$  at 1.6kHz with 8dB maximum passband ripple ( $R_p$ ),
  - Stopband edge frequency  $f_s$  at 2.4kHz with a minimum 16dB stopband attenuation ( $A_s$ ).
- Use the Butterworth lowpass filter and **Bilinear Transformation** method with sampling interval  $T = 0.1$  in the design.

## Example 2 Solution

- Determine the continuous-time critical frequencies  $\Omega_p$  and  $\Omega_s$  by frequency warping of the Bilinear Transformation method with  $F_s = 8000$  Hz.
- The discrete-time critical frequencies are given by

$$\omega_p = \frac{f_p}{F_s} \cdot 2\pi = \frac{1600}{8000} \cdot 2\pi = 0.4\pi \quad \omega_s = \frac{f_s}{F_s} \cdot 2\pi = \frac{2400}{8000} \cdot 2\pi = 0.6\pi$$

- Apply frequency pre-warping to obtain the continuous-time critical frequencies with sampling interval  $T = 0.1$  :

$$\Omega_p = \frac{2}{T} \tan \frac{\omega_p}{2} = \frac{2}{0.1} \tan \left( \frac{0.4\pi}{2} \right) = 14.5309 \text{ rad s}^{-1}$$

$$\Omega_s = \frac{2}{T} \tan \frac{\omega_s}{2} = \frac{2}{0.1} \tan \left( \frac{0.6\pi}{2} \right) = 27.5276 \text{ rad s}^{-1}$$

## Example 2 Solution

- Using the Butterworth order estimation formula, we have

$$N = \left\lceil \frac{\log_{10}[(10^{R_p/10} - 1)/(10^{A_s/10} - 1)]}{2 \log_{10}(\Omega_p/\Omega_s)} \right\rceil = \left\lceil \frac{\log_{10}[(10^{8/10} - 1)/(10^{16/10} - 1)]}{2 \log_{10}(14.5309/27.5276)} \right\rceil = \lceil 1.56 \rceil = 2$$

- With  $N = 2$ , we can obtain the range of analog cutoff frequency  $\Omega_c$  as

$$\Omega_c \in \left[ \frac{\Omega_p}{(10^{R_p/10} - 1)^{1/(2N)}}, \frac{\Omega_s}{(10^{A_s/10} - 1)^{1/(2N)}} \right] = \left[ \frac{14.5309}{(10^{8/10} - 1)^{1/(2 \cdot 2)}}, \frac{27.5276}{(10^{16/10} - 1)^{1/(2 \cdot 2)}} \right] = [9.5725, 11.0289]$$

- For simplicity,  $\Omega_c = 10$  is employed

# Python Code

```
import numpy as np
Rp=8
As=16
Wp= 14.5309
Ws= 27.5276
```

$$N = \left\lceil \frac{\log_{10}[(10^{8/10} - 1)/(10^{16/10} - 1)]}{2 \log_{10}(14.5309/27.5276)} \right\rceil = \lceil 1.56 \rceil = 2$$

```
N = (np.log((pow(10, Rp/10) - 1) / (pow(10, As/10) - 1))) / (2 * np.log(Wp/Ws))
```

```
N
```

```
1.5566977828103328
```

```
import numpy as np
Rp=8
As=16
Wp= 14.5309
Ws= 27.5276
```

$$\Omega_c \in \left[ \frac{14.5309}{(10^{\frac{8}{10}} - 1)^{1/(2 \cdot 2)}}, \frac{27.5276}{(10^{\frac{16}{10}} - 1)^{1/(2 \cdot 2)}} \right] = [9.5725, 11.0289]$$

```
N=2
```

```
Wc1 = Wp / (pow((pow(10, Rp/10) - 1), (1 / (2 * N))))
Wc2 = Ws / (pow((pow(10, As/10) - 1), (1 / (2 * N))))
```

```
Wc1
```

```
9.572549171535371
```

```
Wc2
```

```
11.028855136049335
```

# Normalized Butterworth Filter Transfer Functions

For  $\Omega_c = 1$ , we have the transfer functions of the Butterworth Filters in different order  $N$ .

N	Butterworth Transfer Functions
1	$\frac{1}{s + 1}$
2	$\frac{1}{s^2 + \sqrt{2}s + 1}$
3	$\frac{1}{(s^2 + s + 1)(s + 1)}$
4	$\frac{1}{(s^2 + 0.76536s + 1)(s^2 + 1.84776s + 1)}$
5	$\frac{1}{(s + 1)(s^2 + 0.6180s + 1)(s^2 + 1.6180s + 1)}$

[https://en.wikipedia.org/wiki/Butterworth\\_filter#Normalized\\_Butterworth\\_polynomials](https://en.wikipedia.org/wiki/Butterworth_filter#Normalized_Butterworth_polynomials)



- From the **Table of the Normalized Butterworth Filter Transfer Functions**, we know that the **2<sup>nd</sup>** Order Butterworth Lowpass filter with cutoff frequency  $\Omega_c = 1$  is

$$H_{LP}(s) = \frac{1}{s^2 + \sqrt{2}s + 1}$$

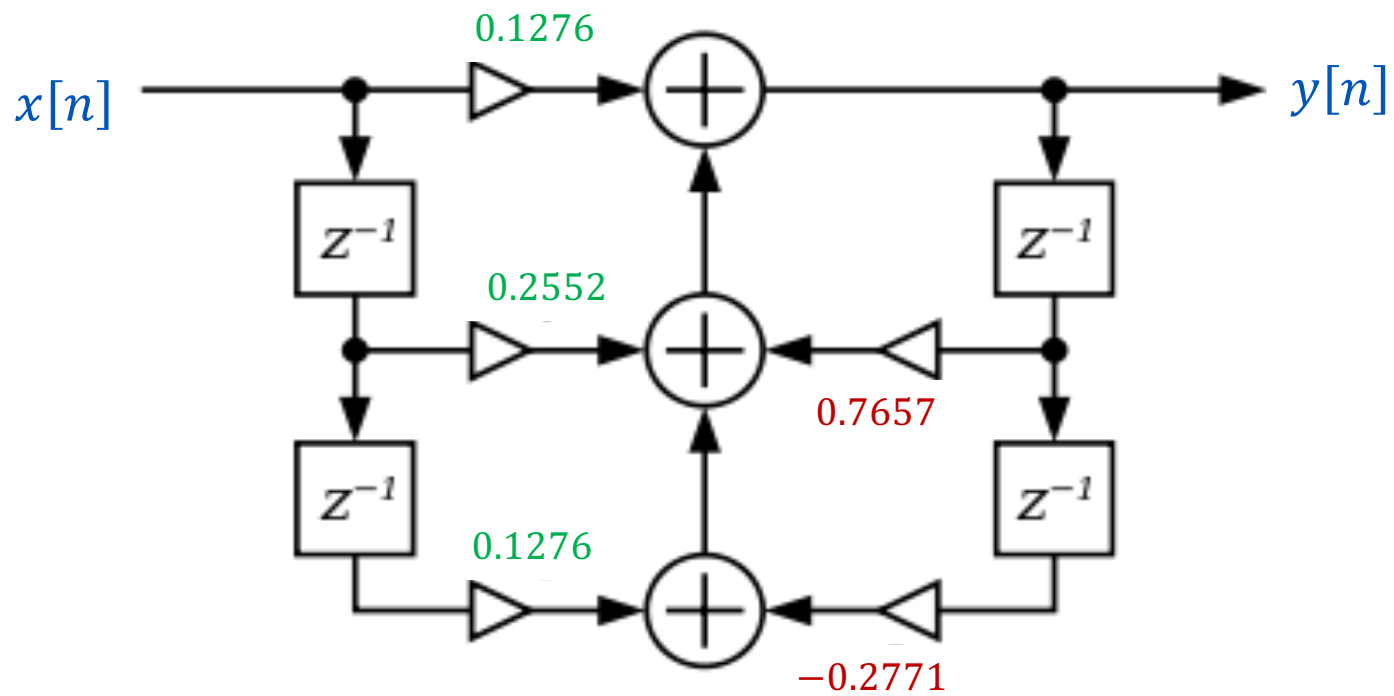
- Then, we map the cutoff frequency of this transfer function to  $\Omega_c = 10$  as

$$H_{LP}(s) = \frac{1}{s^2 + \sqrt{2}s + 1} \Big|_{s=\frac{s}{\Omega_c}} = \frac{1}{\left(\frac{s}{10}\right)^2 + \sqrt{2}\left(\frac{s}{10}\right) + 1} = \frac{100}{s^2 + 10\sqrt{2}s + 100}$$

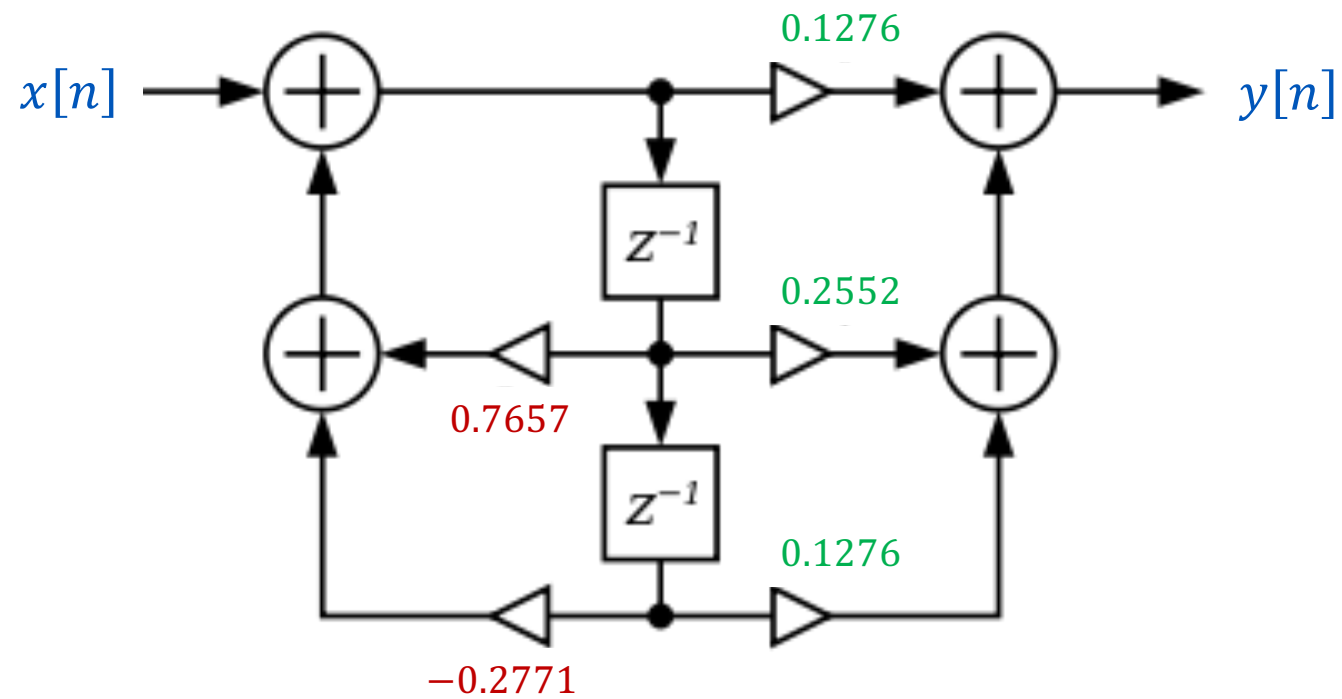
- Finally, we apply the Bilinear Transformation with  $T = 0.1$  to obtain  $H_{LP}(z)$  as

$$\begin{aligned}
 H_{LP}(z) &= H_{LP}(s) \Big|_{s=\frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}} = \frac{100}{\left(\frac{2}{0.1} \cdot \frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 10\sqrt{2} \cdot \frac{2}{0.1} \cdot \frac{1-z^{-1}}{1+z^{-1}} + 100} \\
 &= \frac{1 + 2z^{-1} + z^{-2}}{7.8284 - 6z^{-1} + 2.1716z^{-2}} \\
 &= \frac{0.1276 + 0.2552z^{-1} + 0.1276z^{-2}}{1 - 0.7657z^{-1} + 0.2771z^{-2}}
 \end{aligned}$$

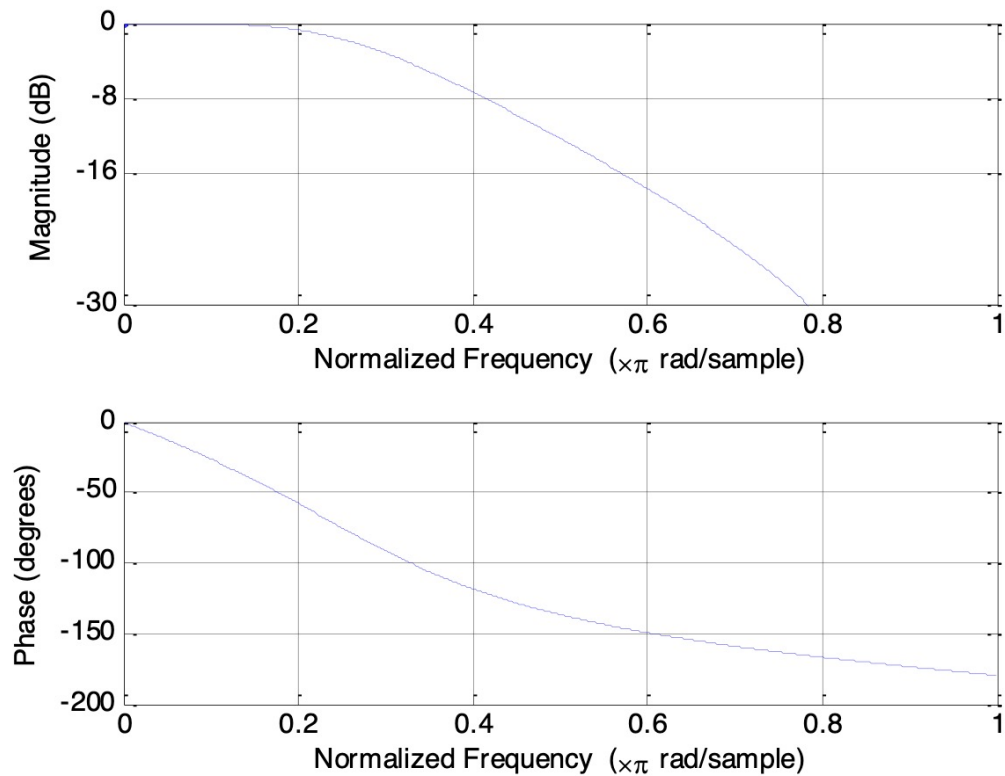
# Direct Form Filter Structure Implementation



# Canonical Form Filter Structure Implementation



# Magnitude and phase responses based on bilinear transformation



## Bilinear Transformation Example 3

- Determine the transfer function  $H_{HP}(z)$  of a digital **highpass** filter whose magnitude requirements are  $\omega_p = 0.4\pi$ ,  $\omega_s = 0.6\pi$ ,  $R_p = 8 \text{ dB}$  and  $A_s = 16 \text{ dB}$ .
- Use the normalized Butterworth lowpass filter and **analog to analog transformation** to the analog highpass transfer function.
- Finally, use **Bilinear Transformation** method with sampling interval  $T = 0.1$  to obtain the  $H_{HP}(z)$ .

## Example 3 Solution

- Based on the results of the Example 2, we know that
  - The order of the filter is **2**
  - The analog cutoff frequency  $\Omega_c = 10$
  - From the **Table of the Normalized Butterworth Filter Transfer Functions**, we know that the 2<sup>nd</sup> Order Butterworth **Lowpass filter** with cutoff frequency  $\Omega_c = 1$  is

$$H_{LP}(s) = \frac{1}{s^2 + \sqrt{2}s + 1}$$

- Now, we can apply Analog-to-Analog Transformation to obtain the **highpass** transfer function  $H_{HP}(s)$  as

$$H_{HP}(s) = H_{LP}(s) \Big|_{s=\frac{\Omega_c}{s}} = \frac{1}{\left(\frac{10}{s}\right)^2 + \sqrt{2}\left(\frac{10}{s}\right) + 1} = \frac{s^2}{s^2 + 10\sqrt{2}s + 100}$$

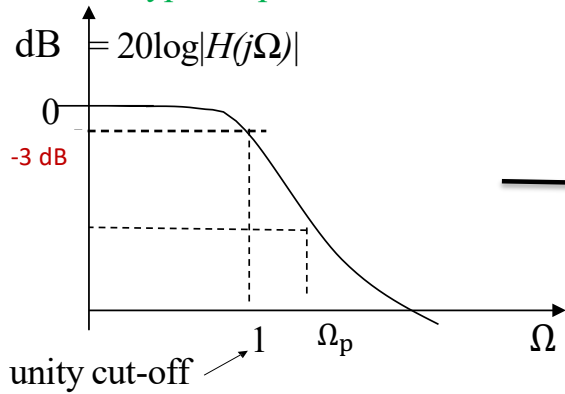
- Finally, we apply the Bilinear Transformation with  $T = 0.1$  to obtain  $H_{HP}(z)$  as

$$\begin{aligned}
 H_{HP}(z) &= H_{HP}(s) \Big|_{s=\frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}} = \frac{s^2}{s^2 + 10\sqrt{2}s + 100} \Big|_{s=\frac{2}{T} \frac{1-z^{-1}}{1+z^{-1}}} \\
 &= \frac{\left(\frac{2}{0.1} \cdot \frac{1-z^{-1}}{1+z^{-1}}\right)^2}{\left(\frac{2}{0.1} \cdot \frac{1-z^{-1}}{1+z^{-1}}\right)^2 + 10\sqrt{2} \cdot \frac{2}{0.1} \cdot \frac{1-z^{-1}}{1+z^{-1}} + 100} = \frac{1 - 2z^{-1} + z^{-2}}{1.9571 - 1.5z^{-1} + 0.5429z^{-2}} \\
 &= \frac{0.5110 - 1.0219z^{-1} + 0.5110z^{-2}}{1 + 0.7664z^{-1} + 0.2774z^{-2}}
 \end{aligned}$$

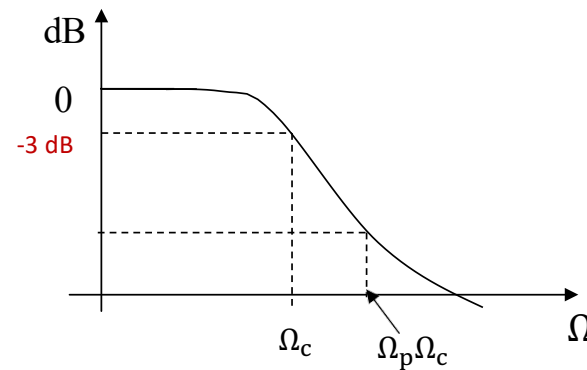


# Analog to Analog Transformation

Butterworth Prototype Response

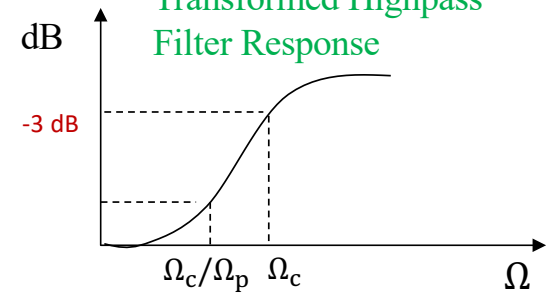


Transformed Lowpass Filter Response



$$s \rightarrow \frac{s}{\Omega_c}$$

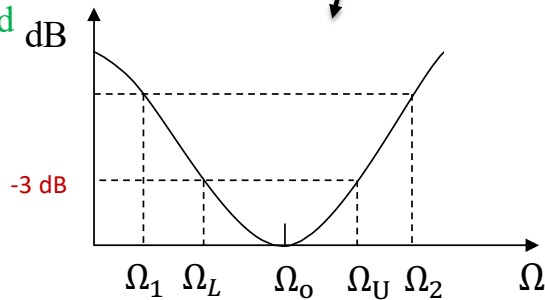
Transformed Highpass Filter Response



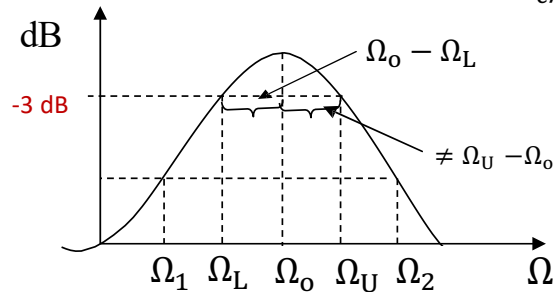
$$s \rightarrow \frac{\Omega_c}{s}$$

$$s \rightarrow \frac{s(\Omega_U - \Omega_L)}{s^2 + \Omega_L\Omega_U}$$

Transformed Bandstop Filter Response



$$s \rightarrow \frac{s^2 + \Omega_L\Omega_U}{s(\Omega_U - \Omega_L)}$$



Transformed Bandpass Filter Response

# **Digital Frequency Band Transformations**

# Digital Frequency Band Transformation

- The operations are like that of the bilinear transformation but now the mapping is performed only in the **z-plane**:

$$z_o^{-1} = T(z^{-1})$$

where  $z_o$  and  $z$  correspond to the **lowpass** and **resultant** filters, respectively, and  $T()$  denotes the **transformation operator**.

- To ensure the transformed filter to be stable and causal, the unit circle of the  $z_o$ -plane should map into those of the  $z$ -plane, respectively.

# Frequency Band Transformation Operators

Filter Type	Transformation Operator	Design Parameter
Lowpass	$z_o^{-1} = \frac{z^{-1} - a}{1 - az^{-1}}$	$a = \frac{\sin\left(\frac{\omega_{c_o} - \omega_o}{2}\right)}{\sin\left(\frac{\omega_{c_o} + \omega_o}{2}\right)}$
Highpass	$z_o^{-1} = -\frac{z^{-1} - a}{1 - az^{-1}}$	$a = -\frac{\cos\left(\frac{\omega_{c_o} + \omega_o}{2}\right)}{\cos\left(\frac{\omega_{c_o} - \omega_o}{2}\right)}$
Bandpass	$z_o^{-1} = \frac{z^{-2} - \frac{2ab}{b+1}z^{-1} + \frac{b-1}{b+1}}{\frac{b-1}{b+1}z^{-2} - \frac{2ab}{b+1}z^{-1} + 1}$	$a = \frac{\cos\left(\frac{\omega_{c_2} + \omega_{c_1}}{2}\right)}{\cos\left(\frac{\omega_{c_2} - \omega_{c_1}}{2}\right)} \quad b = \cot\left(\frac{\omega_{c_2} + \omega_{c_1}}{2}\right) \tan\left(\frac{\omega_{c_o}}{2}\right)$
Bandstop	$z_o^{-1} = \frac{z^{-2} - \frac{2a}{1+b}z^{-1} + \frac{1-b}{1+b}}{\frac{1-b}{1+b}z^{-2} - \frac{2a}{1+b}z^{-1} + 1}$	$a = \frac{\cos\left(\frac{\omega_{c_2} + \omega_{c_1}}{2}\right)}{\cos\left(\frac{\omega_{c_2} - \omega_{c_1}}{2}\right)} \quad b = \cot\left(\frac{\omega_{c_2} - \omega_{c_1}}{2}\right) \tan\left(\frac{\omega_{c_o}}{2}\right)$

# Frequency Band Transformation Example

- Determine the transfer function  $H(z)$  of a digital **highpass filter** whose magnitude requirements are  $\omega_p = 0.6\pi$ ,  $\omega_s = 0.4\pi$ ,  $R_p = 8 \text{ dB}$  and  $A_s = 16 \text{ dB}$ .
- Use the Butterworth lowpass filter and bilinear transformation in the design.

## Use the Results of the Bilinear Transformation Example 2

- Determine the transfer function  $H_{LP}(z)$  of a digital lowpass filter whose magnitude requirements are  $\omega_p = 0.4\pi$ ,  $\omega_s = 0.6\pi$ ,  $R_p = 8 \text{ dB}$  and  $A_s = 16 \text{ dB}$ .
- Use the Butterworth lowpass filter and **Bilinear Transformation** method with sampling interval  $T = 0.1$  in the design.

## Solution

- Using the Example 2 of the Bilinear Transformation, the corresponding lowpass digital filter function  $H_{LP}(z)$  is :

$$H_{LP}(z_o) = \frac{0.1276 + 0.2552z_o^{-1} + 0.1276z_o^{-2}}{1 - 0.7657z_o^{-1} + 0.2771z_o^{-2}}$$

- Assigning **the cutoff frequencies as the midpoints** between the passband and stopband frequencies, we have

$$\omega_{c_o} = \omega_c = \frac{0.4\pi + 0.6\pi}{2} = 0.5\pi$$

- Using the Table, the corresponding value of  $a$  is

$$a = -\frac{\cos\left(\frac{\omega_{c_o} + \omega_o}{2}\right)}{\cos\left(\frac{\omega_{c_o} - \omega_o}{2}\right)} = -\frac{\cos(0.5\pi)}{\cos(0)} = 0$$

which gives the transformation operator:

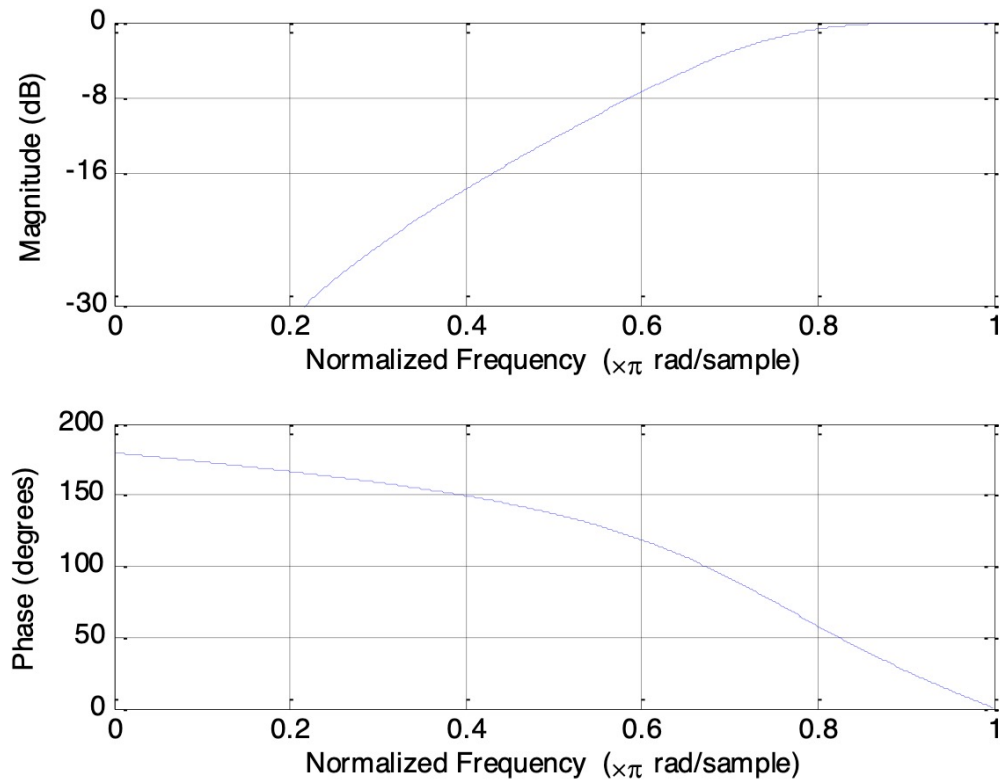
$$z_o^{-1} = -\frac{z^{-1} - a}{1 - az^{-1}} = -z^{-1}$$

- As a result, the digital **highpass** filter transfer function is:

$$H_{HP}(z) = H_{LP}(z_o) \Big|_{z_o^{-1} = -z^{-1}} = \frac{0.1276 - 0.2552z^{-1} + 0.1276z^{-2}}{1 + 0.7657z^{-1} + 0.2771z^{-2}}$$



# Magnitude and phase responses based on frequency band transformation



# Digital Highpass Butterworth Filter to Remove a Single Tone from a Signal

- Generate a signal made up of 10 Hz and 20 Hz, sampled at 1 kHz.
- Design a digital highpass filter at 15 Hz to remove the 10 Hz tone and apply it to the signal.
- **It's recommended to use second-order sections (SOS) format when filtering, to avoid numerical error with transfer function (ba) format)**

```
t = np.linspace(0, 1, 1000, False) # 1 second
sig = np.sin(2*np.pi*10*t) + np.sin(2*np.pi*20*t)

sos = signal.butter(10, 15, 'hp', fs=1000, output='sos')
filtered = signal.sosfilt(sos, sig)

fig, (ax1, ax2) = plt.subplots(2, 1, sharex=True)
ax1.plot(t, sig)
ax1.set_title('10 Hz and 20 Hz sinusoids')
ax1.axis([0, 1, -2, 2])

ax2.plot(t, filtered)
ax2.set_title('After 15 Hz highpass filter')
ax2.axis([0, 1, -2, 2])
ax2.set_xlabel('Time [seconds]')
plt.tight_layout()
plt.show()
```

